

JAEA NDC

**Covariance Evaluation of
Self-Shielding Factor
and
Its Temperature Gradient for
Uncertainty Evaluation of Doppler Reactivity**

ERRORF collaboration

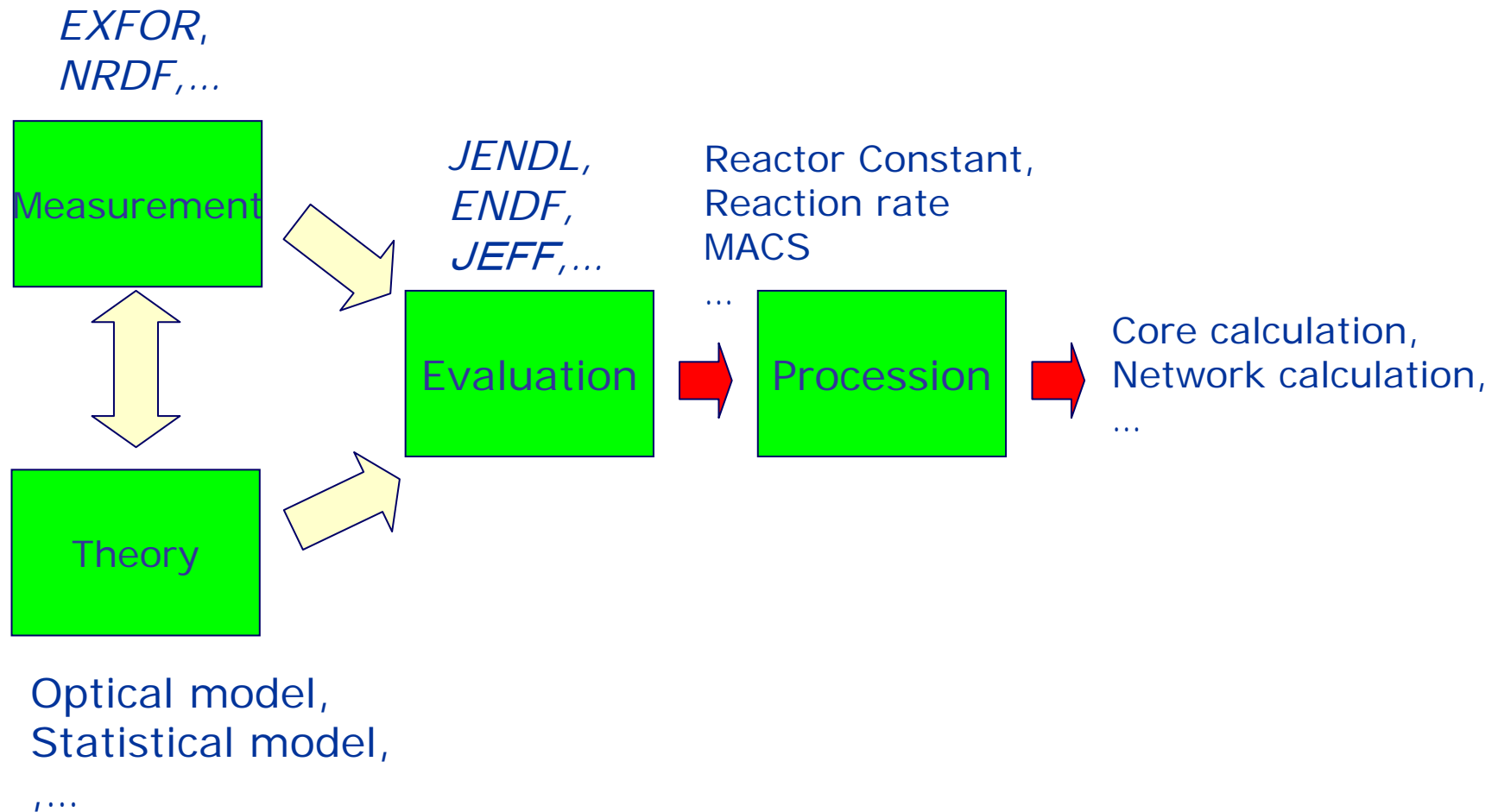
Collaboration

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Contents

- **Doppler reactivity**
- **Covariance evaluation of α -value**
- **Uncertainty in Doppler reactivity using covariances from ERRORF**

Flow of nuclear data

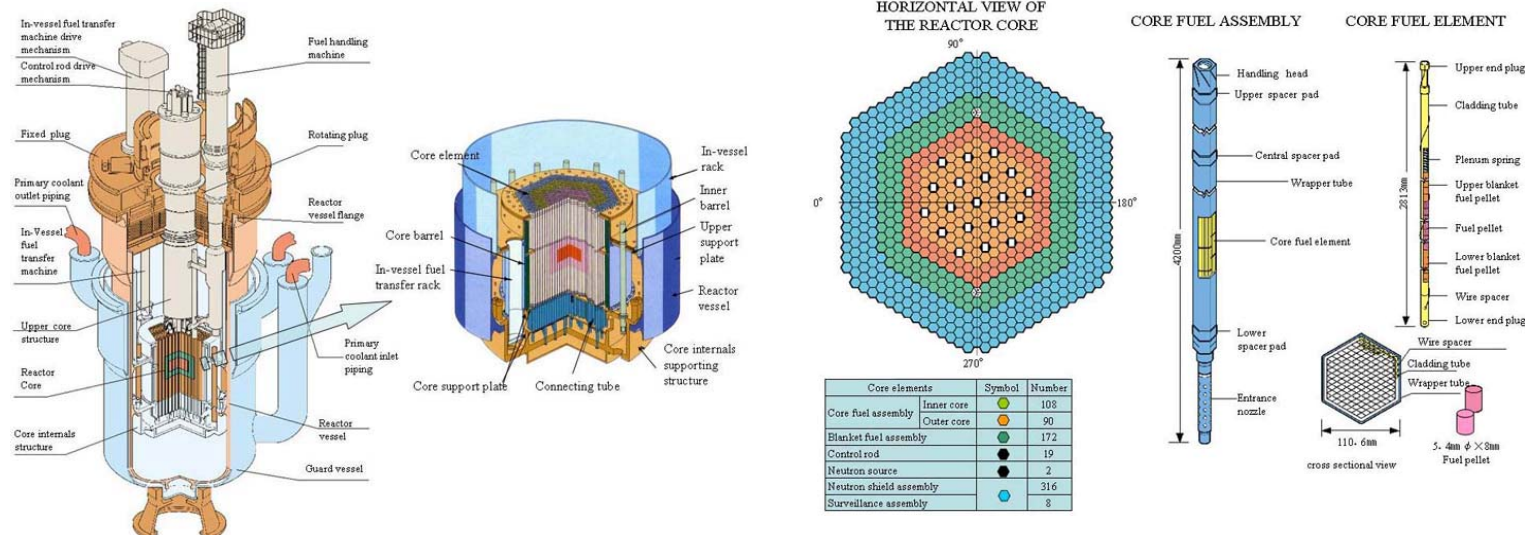


Doppler Reactivity and Nuclear Data



Fast breeder reactor calculation

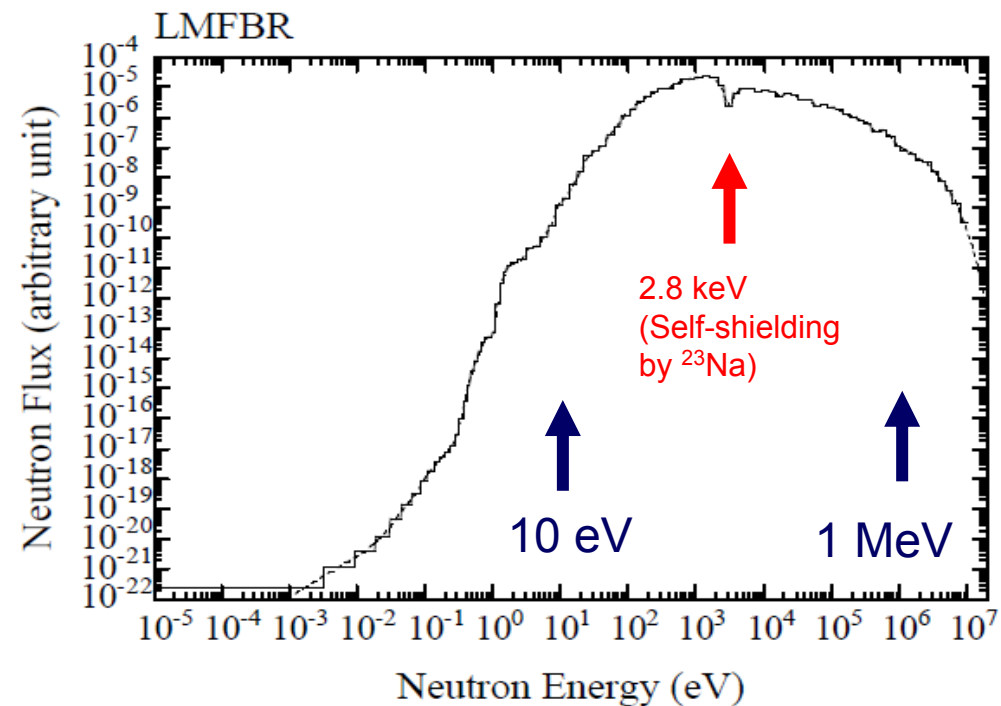
- **Complicated inhomogeneous structure (pellet, cladding tube, wrapper tube etc.)**



**Uncertainty in prediction:
group structure, burning chain, 3D effect...**

Fast breeder reactor and nuclear data

- Energy spectrum of fast breeder reactor



**Nuclear data in wide neutron energy (10^2 eV \sim 10^6 eV)
also could be a source of uncertainty in prediction**

Reactor core parameters

- **Criticality (k_{eff}) (+/- 3%, 1σ)**
- **Sodium void reactivity worth (+/- 20%, 2σ)**
- **Doppler reactivity worth (+/- 14%, 2σ)**
- ...

Doppler reactivity is an important safety parameter in **self-regulation characteristics** of reactors.

Criticality and reactivity worth (Definition)

- **Criticality (k_{eff}):**

ratio of

of incoming neutron per unit time (e.g. fission neutron)

to

of expended neutron per unit time (e.g. fission, capture)

$$k_{\text{eff}} \cong \frac{\int dE \nu(E) \sigma_{\text{fission}}(E) \phi(E)}{\int dE [\sigma_{\text{capture}}(E) + \sigma_{\text{fission}}(E)] \phi(E)}$$

$k_{\text{eff}} = 1$ (critical), < 1 (subcritical), > 1 (supercritical)

Criticality and reactivity worth (Definition)

- **Reactivity worth (ρ) - change of reactivity:**

$$\rho = \Delta p = \frac{1}{k_{\text{eff}}(1)} - \frac{1}{k_{\text{eff}}(2)}$$

for Temperature change 1→2

Example:

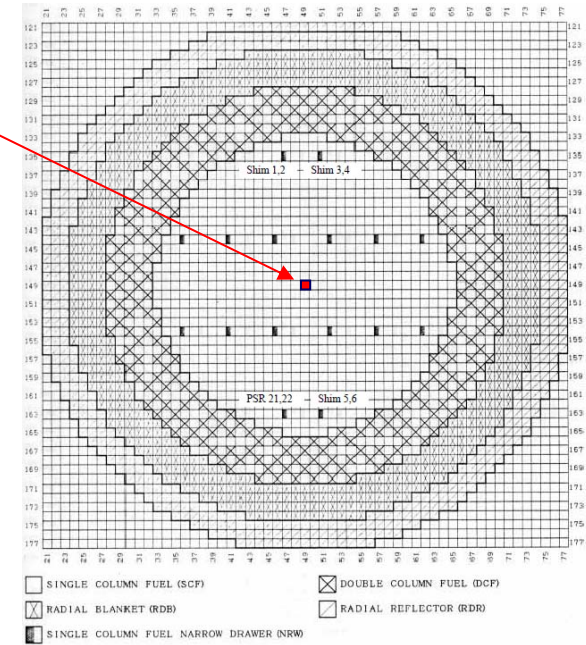
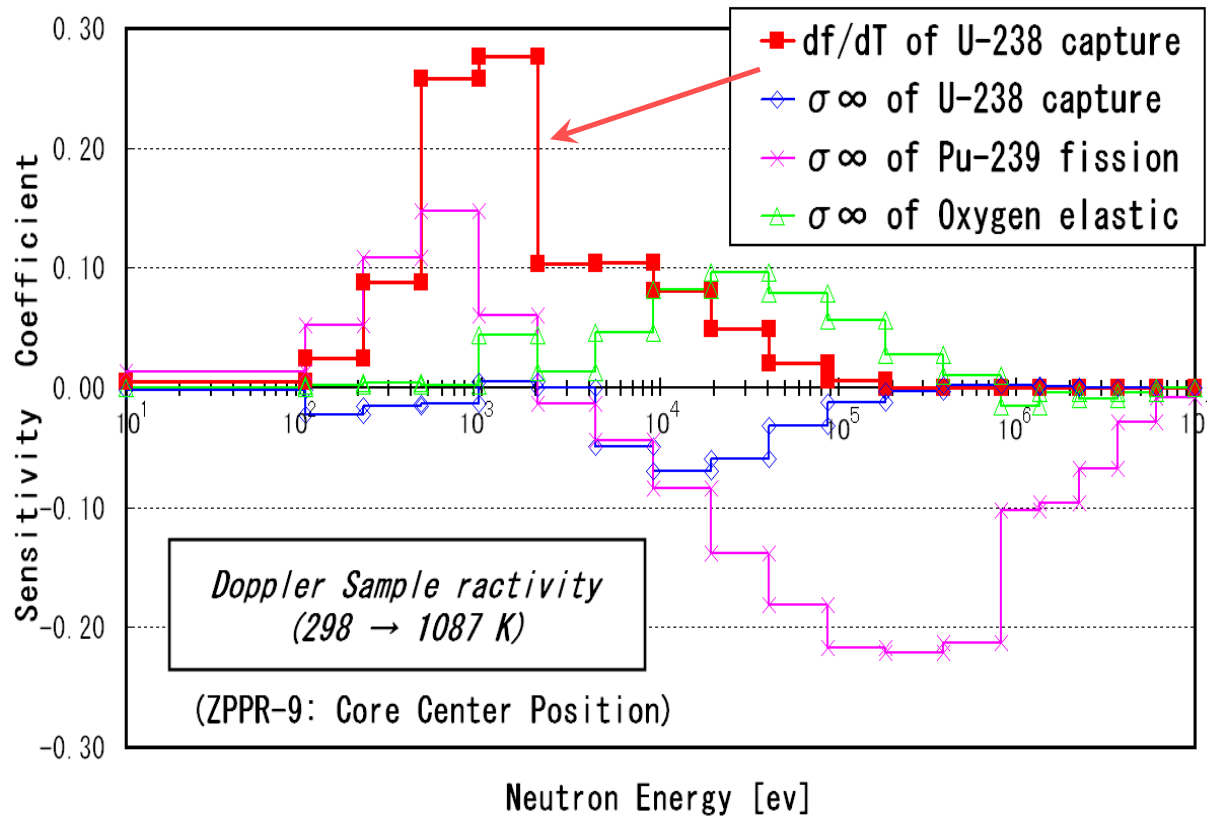
$$\rho = \Delta p = \frac{1}{k_{\text{eff}}(T_{\text{low}})} - \frac{1}{k_{\text{eff}}(T_{\text{high}})}$$

for Temperature change $T_{\text{low}} \rightarrow T_{\text{high}}$

Doppler reactivity worth

Sensitivity for a Sample Doppler Reactivity (ZPPR-9)

(* Sample material: Natural uranium dioxide, app. 1 kg)



(by M.Ishikawa)

Covariance Evaluation of α -value for Doppler Reactivity Uncertainty

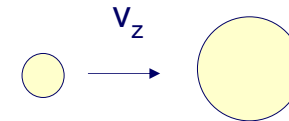
N. Otuka, A. Zukeran, H. Takano, G. Chiba, M. Ishikawa,
J.Nucl.Sci.Technol.Vol.45 No.3 (in press)



Temperature dependence of cross section

- Doppler broadening (single-level Breit-Wigner)

$$\sigma_{\gamma}(E, T) = \sigma_0 \left(\frac{\Gamma_{\gamma}}{\Gamma} \right) \sqrt{\frac{E_0}{E}} \sqrt{\frac{m}{2\pi kT}} \int_{-\infty}^{\infty} \frac{\exp\left(-\frac{E_c}{kT}\right)}{1 + \left(\frac{2(E_c - E_0)}{\Gamma_{\text{tot}}}\right)^2} dv_z$$

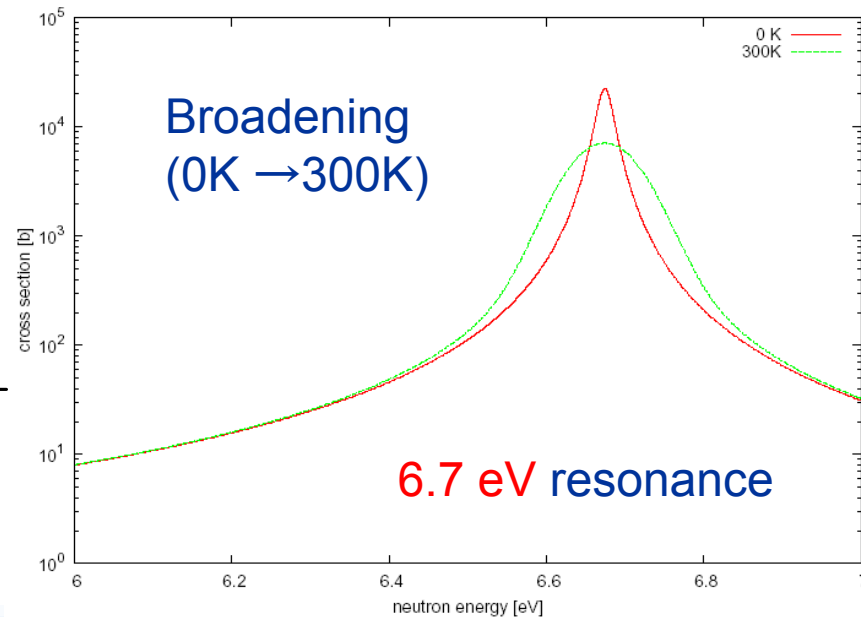


Change in self-shielding effect f:

$$f^g(T, \sigma_b) = \frac{\sigma_{\text{eff}}^g(T, \sigma_b)}{\sigma_{\text{eff}}^g(T_0, \sigma_b = \infty)}$$

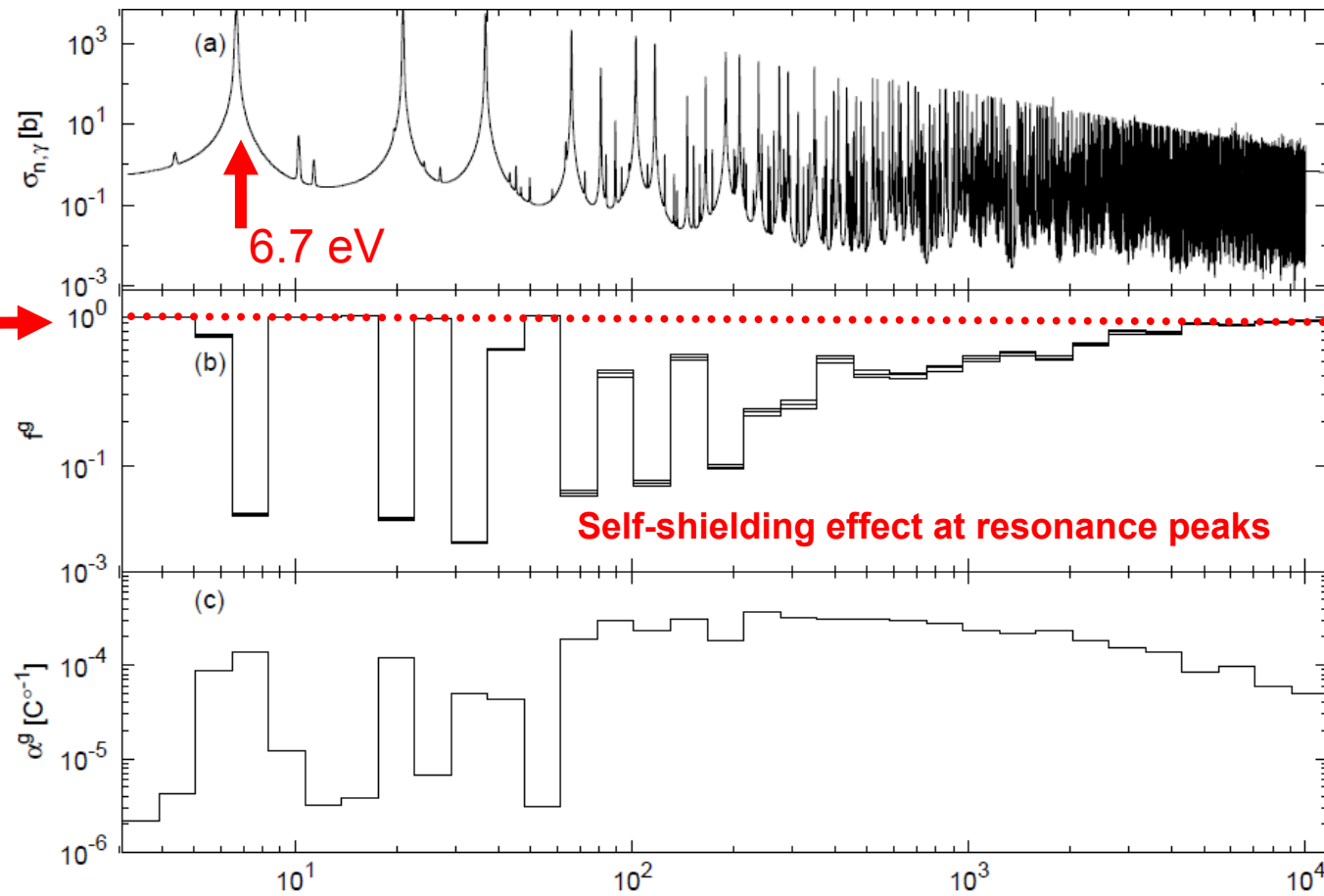
, where $\sigma_{\text{eff}} = \frac{\int dE \sigma(E, T) \phi(E, T, \sigma_b)}{\int dE \phi(E, T, \sigma_b)}$

JENDL-3.3 $^{238}\text{U}(n, \gamma)^{239}\text{U}$ cross section



Example: $^{238}\text{U}(n,\gamma)^{239}\text{U}$ @ 800 deg-K

Cross section



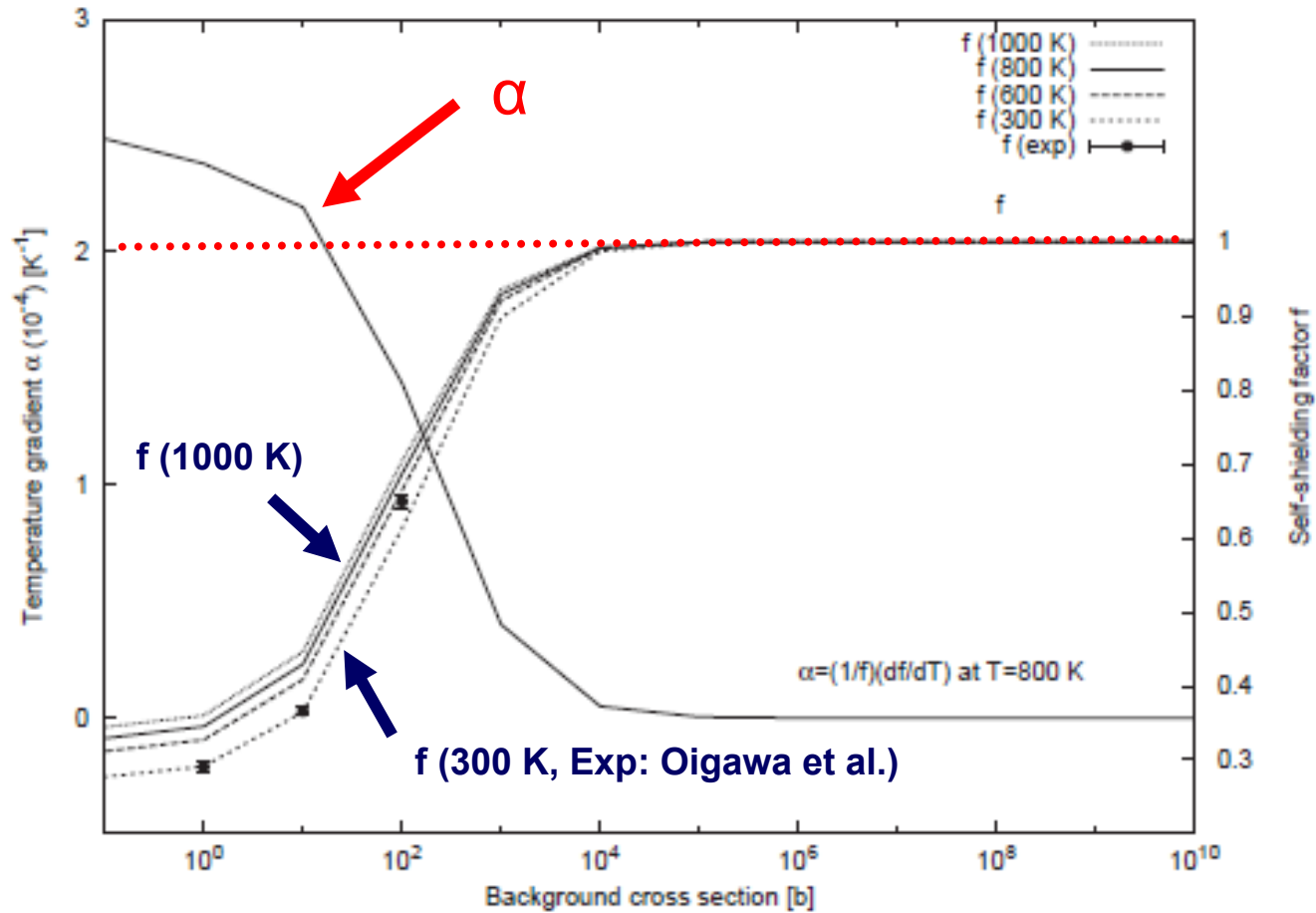
$f=1$ (no self-shielding) →

Self-shielding factor (f-factor)

Temperature gradient of f-factor (α -value):

$$\alpha = (1/f) \left(\frac{\partial f}{\partial T} \right)$$

Example of f and α (^{238}U capture, ~ 1 keV)



Error of reactivity worth and nuclear data

- Doppler reactivity worth: $\rho = \rho(\sigma_{\text{eff}}(T_0), f(T), \alpha(T), \dots)$

Error propagation

from temperature gradient α to Doppler reactivity worth ρ

$$\frac{\Delta\rho}{\rho} = S_{\alpha} \frac{\Delta\alpha}{\alpha}$$

S_{α} can be calculated from sensitivity of criticality at high temperature $S_{k_{\text{eff}}}(T_{\text{high}})$:

$$S_{\alpha} = \left(\frac{\sigma_{\text{eff}}(T_{\text{high}}) - \sigma_{\text{eff}}(T_{\text{low}})}{\sigma_{\text{eff}}(T_{\text{high}})} \right) \times \frac{1}{\rho} \times \frac{S_{k_{\text{eff}}}(T_{\text{high}})}{k_{\text{eff}}(T_{\text{high}})}, \text{ where}$$
$$\frac{\Delta k_{\text{eff}}(T_{\text{high}})}{k_{\text{eff}}(T_{\text{high}})} = S_{k_{\text{eff}}}(T_{\text{high}}) \frac{\Delta\sigma_{\text{eff}}(T_{\text{high}})}{\sigma_{\text{eff}}(T_{\text{high}})}$$

$\Delta\alpha(T)$: from uncertainty in nuclear data (Our work!)

Uncertainty in temperature gradient

- Error propagation from nuclear data to temperature gradient α

$$\left(\frac{\Delta \alpha^g}{\alpha^g} \right)^2 = \sum_{i,j} S^g_i S^g_j \rho_{ij} \frac{\Delta x_i}{x_i} \frac{\Delta x_j}{x_j} \rightarrow \frac{\Delta \alpha^g}{\alpha^g} \cong \sum_{i,j} S^g_i \frac{\Delta x_i}{x_i}$$

$\rho_{ij} \Delta x_i \Delta x_j$: covariance of resonance parameter ($E_r, \Gamma_n, \Gamma_\gamma, \Gamma_f$)

... evaluated in JENDL ($^{235}\text{U}, ^{238}\text{U}, ^{239}\text{Pu}, ^{240}\text{Pu}, \dots$)

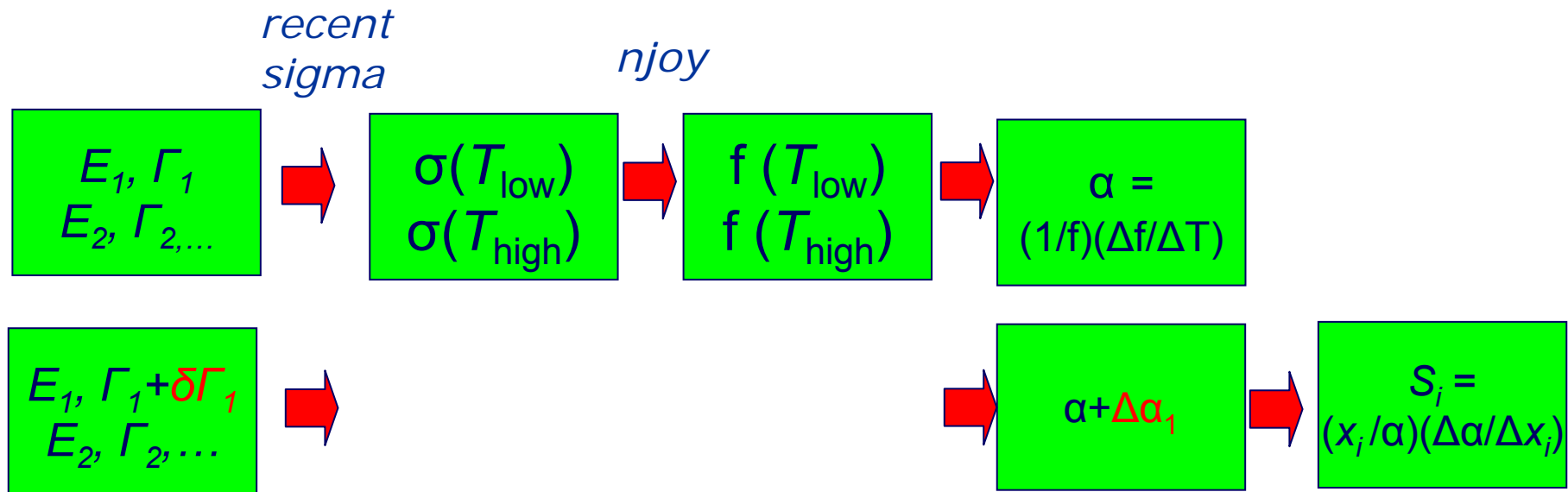
$$S^g_i = \frac{x_i}{\alpha^g} \frac{\partial \alpha^g}{\partial x_i}$$

S_i : Sensitivity coefficient of x_i to α

Covariance of resonance parameter (U, Np, Pu)

Nuclide	Library
^{233}U	JENDL-3.3, JEFF-3.1
^{235}U	JENDL-3.3
^{238}U	JENDL-3.3
^{237}Np	JENDL-3.3
^{238}Pu	JENDL-3.3
^{239}Pu	JENDL-3.3
^{240}Pu	JENDL-3.3, ENDF-B/VI
^{241}Pu	JENDL-3.3
^{242}Pu	JENDL-3.3, ENDF-B/VI

Flow of calculation to obtain $\Delta\alpha$ (*ERRORF*)



... repeat for all resonances (561 s-wave levels for ^{238}U)

$$\Rightarrow \left(\frac{\Delta\alpha}{\alpha} \right)^2 = \sum_{i,j} S_i S_j \rho_{ij} \frac{\Delta x_i}{x_i} \frac{\Delta x_j}{x_j}$$

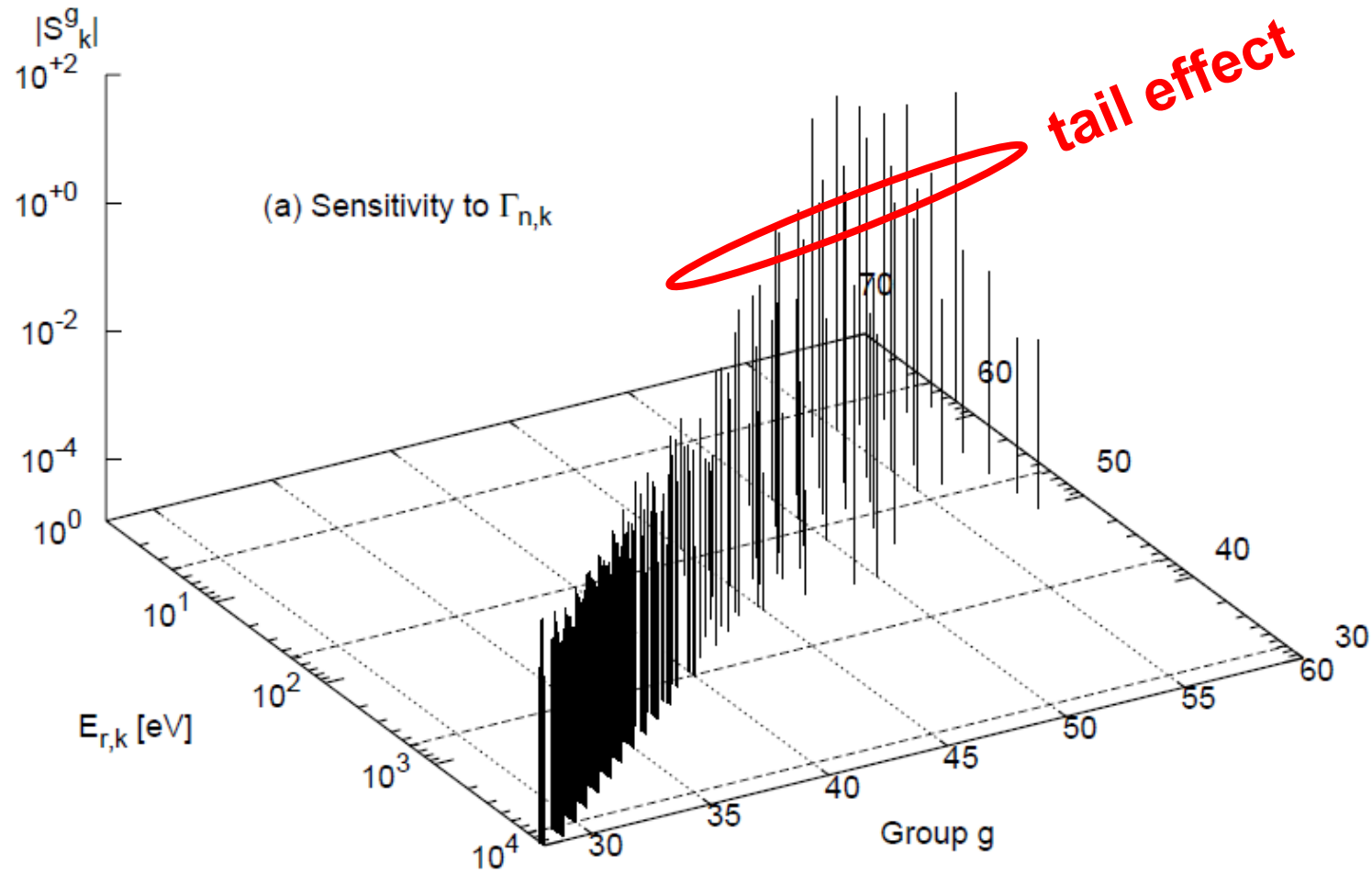
($\rho_{ij} \Delta x_i \Delta x_j$ are from covariance in JENDL)

A new system "*ERRORF*"

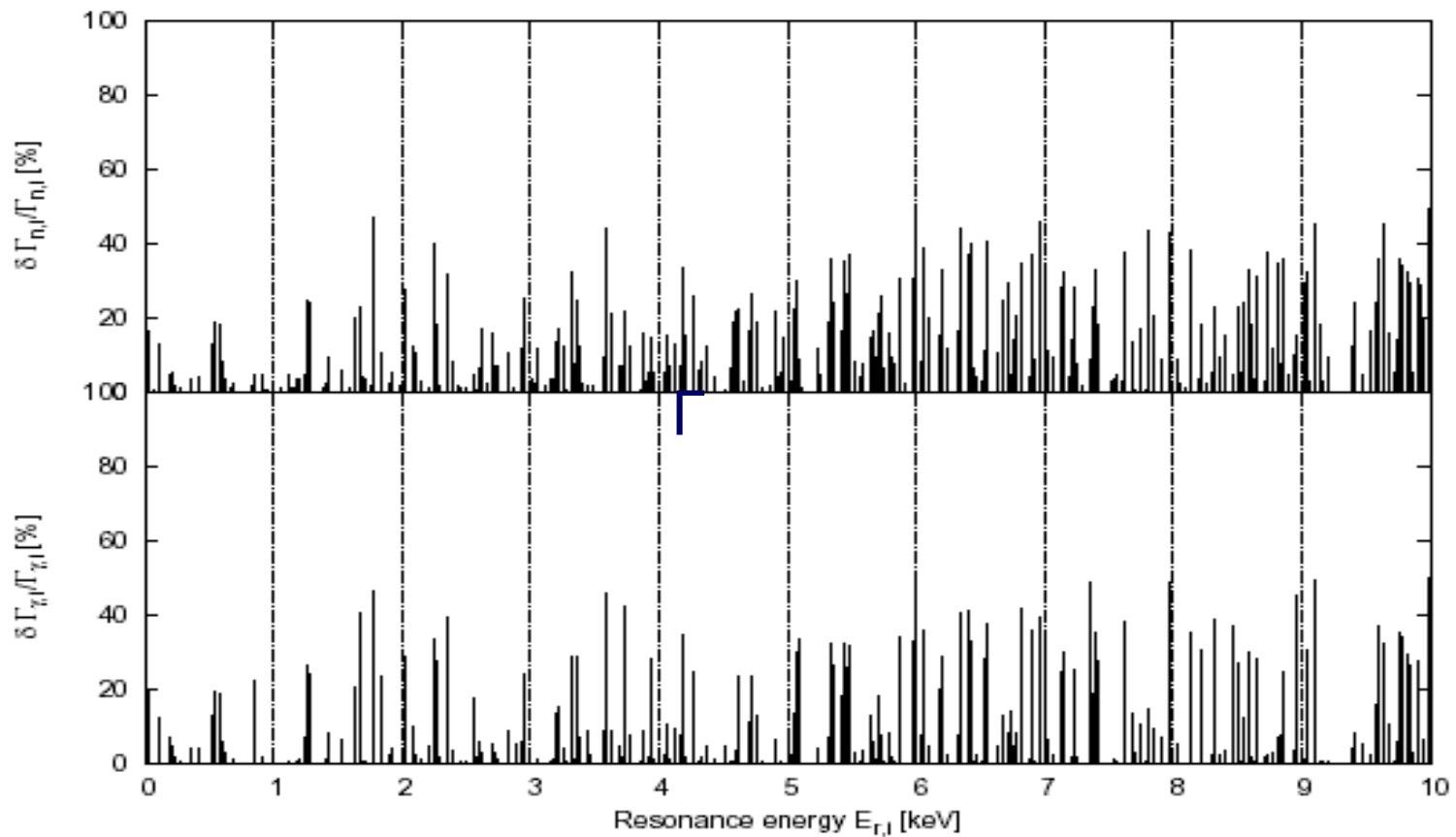
JAEA Nuclear Data Centre



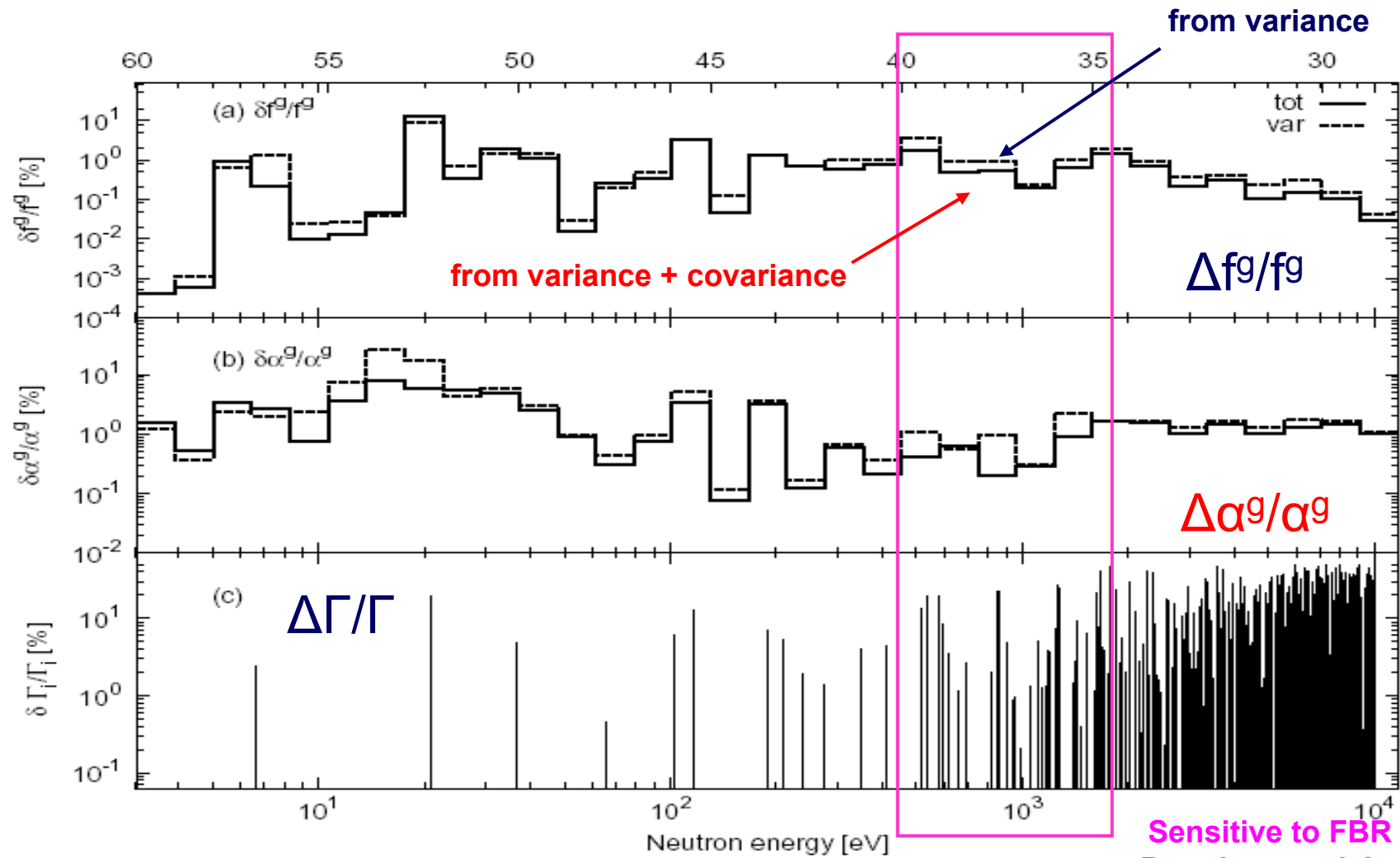
Sensitivity $S_i^g = (\Gamma_n / \alpha) (\Delta\alpha / \Delta\Gamma_n)$



$\Delta\Gamma_n$ and $\Delta\Gamma_\gamma$ of ^{238}U in JENDL-3.3



$\Delta\alpha^g/\alpha^g$ (in JFS 60 group structures)



$T=800\text{K}$, $\sigma_b=37$ barn

$\Delta\alpha^g/\alpha^g$ (in JFS 60 group structures)

Gr	E_{\max} [eV]	f	$\delta f^g/f^g$ [%]		α ($10^{-4}/\text{K}$)	$\delta\alpha^g/\alpha^g$ [%]	
			tot	var		tot	var
...	...	Unresolved resonance region $\Delta\alpha^g/\alpha^g$					
27	1.5034E+04						
28	1.1709E+04	0.9444	0.0289	0.0437	0.3813	1.0054	1.0776
29	9.1188E+03	0.9258	0.1017	0.1490	0.4481	1.4260	1.6756
30	7.1017E+03	0.8792	0.1488	0.3142	0.7400	1.2854	1.7108
31	5.5308E+03	0.8913	0.1080	0.2258	0.6509	1.0125	1.3370
32	4.3074E+03	0.7721	0.3064	0.4182	1.1065	1.4537	1.6364
33	3.3546E+03	0.7877	0.2242	0.3687	1.2258	1.0435	1.3294
34	2.6126E+03	0.6534	0.6841	0.9353	1.4786	1.5242	1.6700
35	2.0347E+03	0.5290	1.3905	1.9059	1.8930	1.6642	1.6645
36	1.5846E+03	0.5724	0.6365	1.0292	1.7635	0.9159	2.2293
37	1.2341E+03	0.5227	0.1913	0.2321	1.9270	0.2856	0.2994
38	9.6112E+02	0.4546	0.5194	0.9475	2.3185	0.1997	0.9847
39	7.4852E+02	0.4065	0.5080	0.8958	2.4933	0.6442	0.5627
40	5.8295E+02	0.4154	1.7276	3.7449	2.5972	0.4129	1.0545
41	4.5400E+02	0.5179	0.7790	1.0278	2.5550	0.2084	0.3675

Sensitive to FBR
Doppler reactivity

var+cov var

$T=800\text{K}$, $\sigma_b=37$ barn

Covariance of α (in JFS 60 group structures)

$$A = SVS^t$$

A: covariance of α

S: sensitivity

V: covariance of (E, Γ)

Gr	28	29	30	31	32	33	34	35	36	37	38	39	40	41
28	100	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	100	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	100	1	0	0	0	0	0	0	0	0	0	0
31	0	0	1	100	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	100	-13	0	0	0	0	0	0	0	0
33	0	0	0	0	-13	100	1	0	0	0	0	0	0	0
34	0	0	0	0	0	1	100	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	100	-1	0	0	0	0	0
36	0	0	0	0	0	0	0	-1	100	-3	0	0	0	0
37	0	0	0	0	0	0	0	0	-3	100	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	100	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	100	-92	0
40	0	0	0	0	0	0	0	0	0	0	0	-92	100	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	100
42	0	0	0	0	0	0	0	0	0	0	0	0	1	12
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0	1	1
45	0	0	0	0	0	0	0	0	0	0	0	1	0	-3
46	0	0	0	0	0	0	0	0	0	0	0	0	0	0
47	0	0	0	0	0	0	0	0	0	0	0	0	0	0
48	0	0	0	0	0	0	0	0	0	0	0	0	0	0
49	0	0	0	0	0	0	0	0	0	0	0	1	0	-3
50	0	0	0	0	0	0	0	0	0	0	0	0	0	0
51	0	0	0	0	0	0	0	0	0	0	0	0	0	0
52	0	0	0	0	0	0	0	0	0	0	0	0	0	1
53	0	0	0	0	0	0	0	0	0	0	0	0	0	0
54	0	0	0	0	0	0	0	0	0	0	0	0	0	0
55	0	0	0	0	0	0	0	0	0	0	0	0	0	0
56	0	0	0	0	0	0	0	0	0	0	0	0	0	0
57	0	0	0	0	0	0	0	0	0	0	0	0	0	0
58	0	0	0	0	0	0	0	0	0	0	0	0	0	0
59	0	0	0	0	0	0	0	0	0	0	0	0	0	0
60	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Sensitive to FBR
Doppler reactivity

T=800K, $\sigma_b=37$ barn

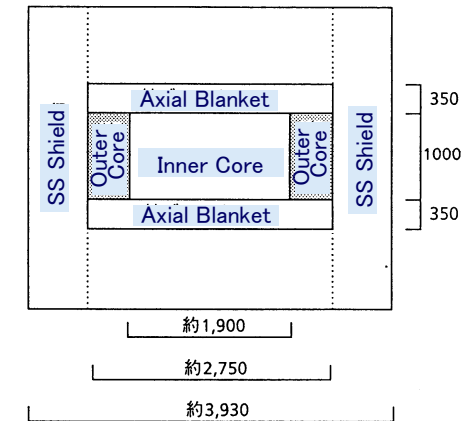
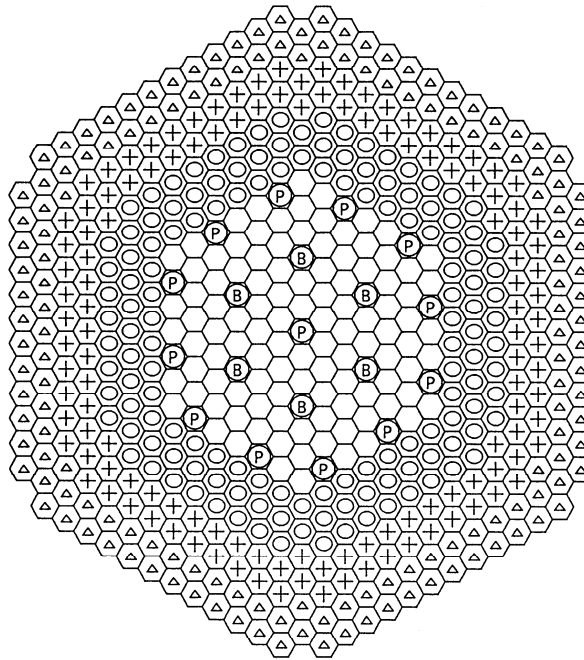
Doppler Reactivity Uncertainty Evaluation

(a 600 MWe-Class Sodium-Cooled FBR)

(from Ishikawa-san)

Specification of a 600 MWe-class FBR

- Thermal power :
1,600MWt
- Operating cycle: 365 days
- Pu ratio (Inner/Outer core) :
16.5/20.5 %
- Pu composition ($^{238}/^{239}$
 $/^{240}/^{241}/^{242}$) : 3/53/25/12/7
- Burnup reactivity loss :
2.5 %dk/kk'/cycle
- Doppler Coefficient
(BOEC) : $-8.0E-3$ Tdk/dT
- Sodium void reactivity
(whole core, BOEC): 4.6 \$
- Prompt neutron lifetime
(BOEC) : 0.41 micro-sec
- Beta effective (BOEC) :
3.8E-3



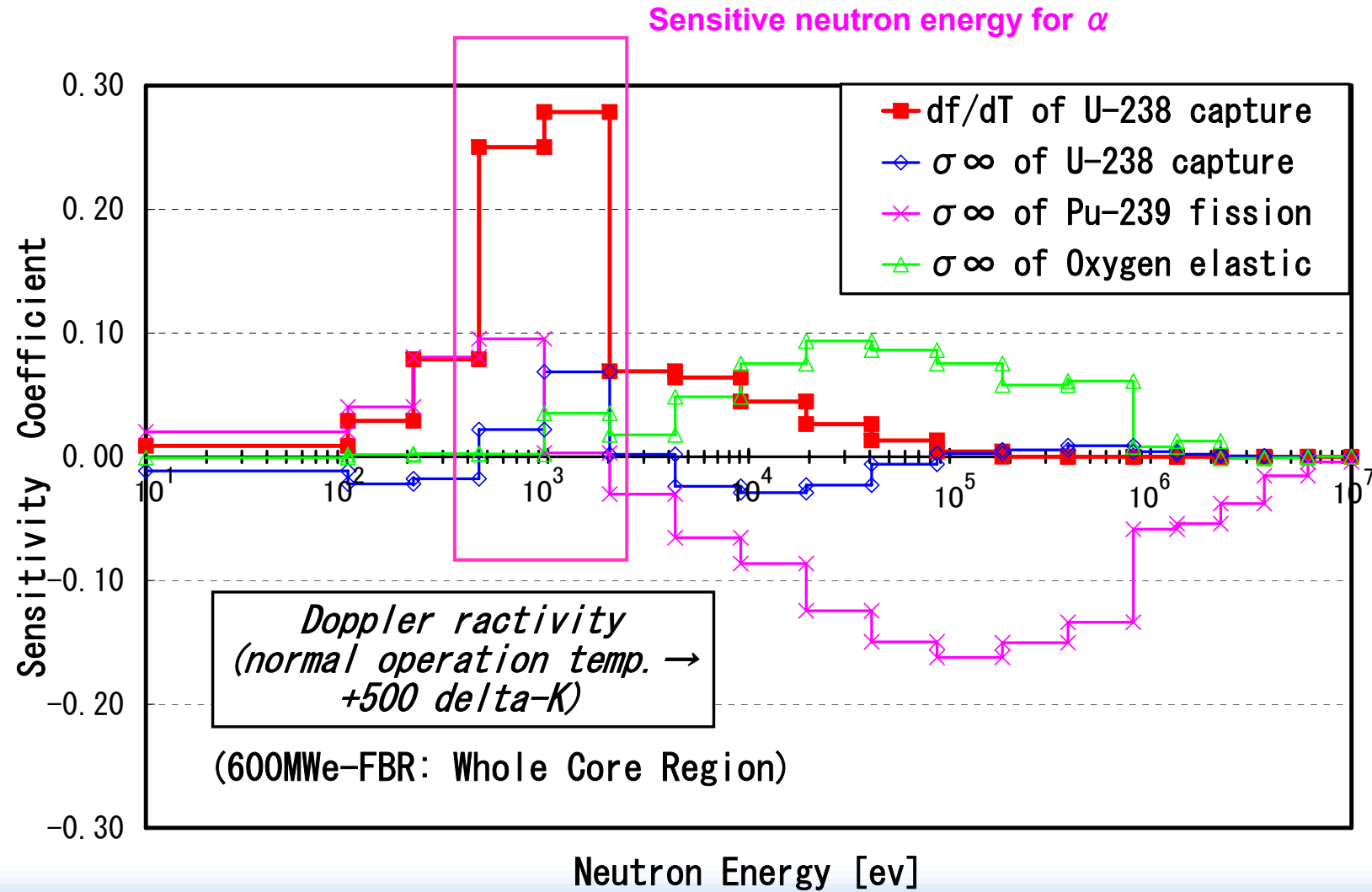
(Diameter(mm))

⬡	Inner Core	108
⊙	Outer Core	138
⊕	SS Shield	126
△	B4C Shield	150
Ⓟ	Primary CR	13
Ⓟ	Backup CR	6

Total 541

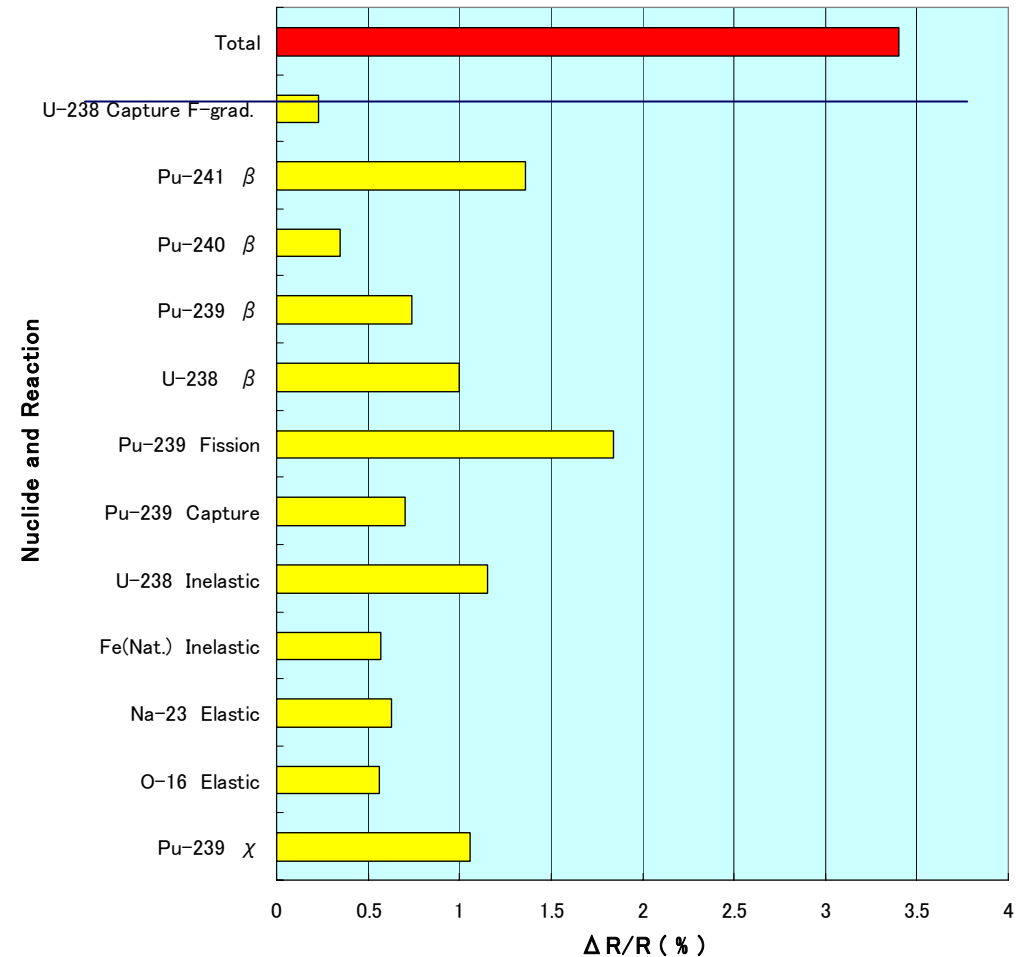
A 600MWe-class FBR Core

Sensitivity of Doppler Reactivity of a 600MWe-class FBR



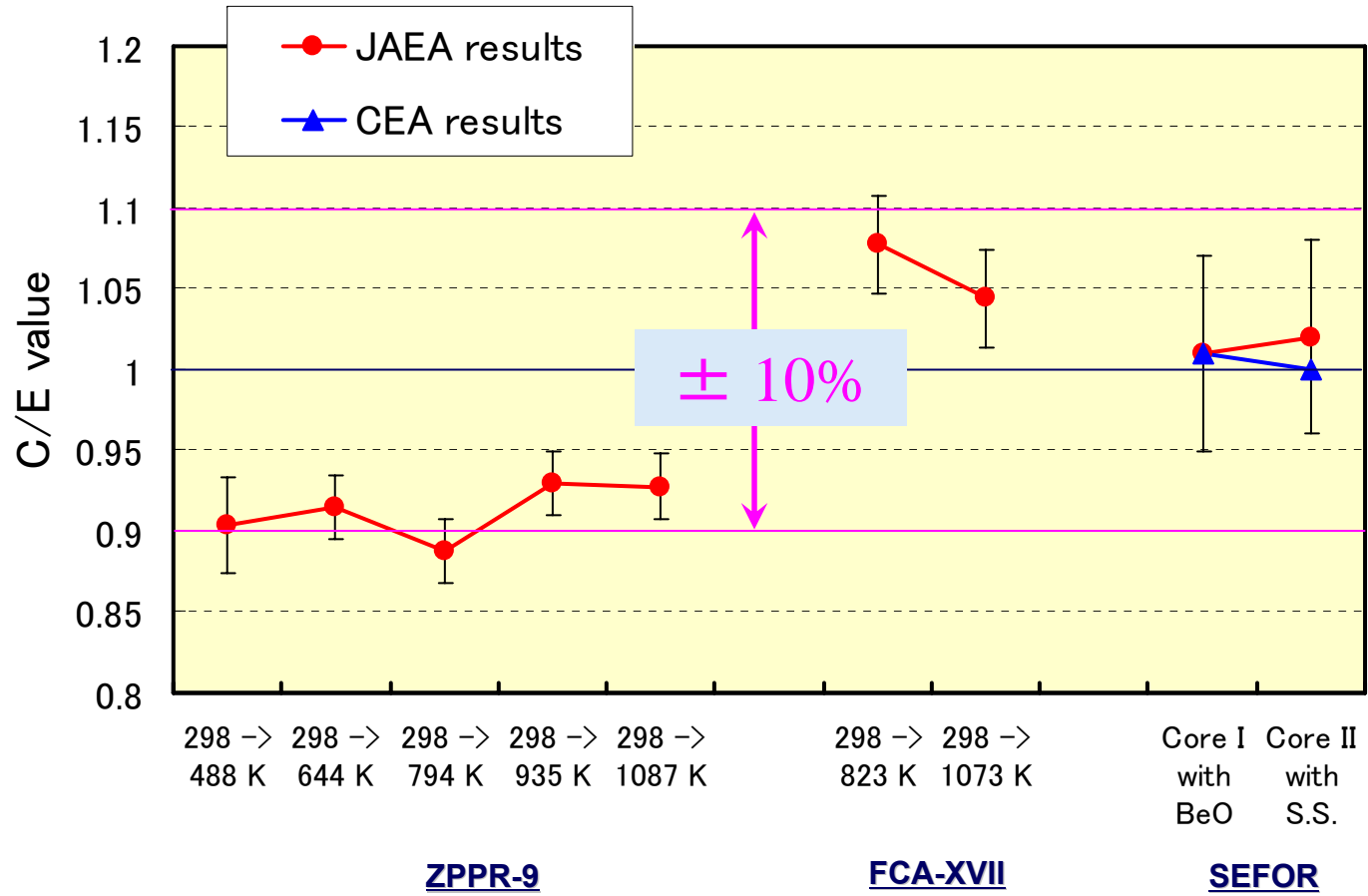
Result of uncertainty in Doppler reactivity

No.	Nuclide and Reaction	$\Delta R/R$ (%)	Contribution (%)
1	Pu-239 χ	1.06	9.7
2	C-12 Capture	0	0.0
3	O-16 Elastic	0.56	2.7
4	O-16 Inelastic	0.01	0.0
5	O-16 μ	0.02	0.0
6	Na-23 Capture	0.26	0.6
7	Na-23 Elastic	0.63	3.4
8	Na-23 Inelastic	0.07	0.0
9	Na-23 μ	0.03	0.0
10	Cr (Nat.) μ	0.01	0.0
11	Fe (Nat.) Capture	0.14	0.2
12	Fe (Nat.) Elastic	0.34	1.0
13	Fe (Nat.) Inelastic	0.57	2.8
14	Fe (Nat.) μ	0.05	0.0
15	Ni (Nat.) μ	0.01	0.0
16	U-235 Capture	0.03	0.0
17	U-235 Fission	0.05	0.0
18	U-235 ν	0.01	0.0
19	U-235 Inelastic	0.01	0.0
20	U-238 Capture	0.24	0.5
21	U-238 Fission	0.11	0.1
22	U-238 ν	0.14	0.2
23	U-238 Elastic	0.11	0.1
24	U-238 Inelastic	1.15	11.4
25	U-238 μ	0.01	0.0
26	Pu-239 Capture	0.70	4.2
27	Pu-239 Fission	1.84	29.3
28	Pu-239 ν	0.15	0.2
29	Pu-239 Inelastic	0.27	0.6
30	Pu-239 μ	0	0.0
31	Pu-240 Capture	0.13	0.1
32	Pu-240 Fission	0.22	0.4
33	Pu-240 ν	0.14	0.2
34	Pu-241 Capture	0.08	0.1
35	Pu-241 Fission	0.26	0.6
36	Pu-241 ν	0.02	0.0
37	U-235 χ	0.02	0.0
38	FP (Pu-239) Capture	0	0.0
39	U-235 β	0.04	0.0
40	U-238 β	1.00	8.7
41	Pu-239 β	0.74	4.7
42	Pu-240 β	0.35	1.1
43	Pu-241 β	1.36	16.0
44	Pu-242 β	0.23	0.5
45	U-238 Capture F-grad.	0.23	0.5
Total		3.40	100.0



(a 600 MWe FBR, 500 delta-K)

C/E Values of Doppler Reactivity Measurement



*Small Sample
Doppler Experiment*

*Whole-core
Doppler Experiment*



Conclusion



Conclusion

- **“ERRORF” code is now available:
To evaluate covariance of temperature gradient of self-shielding factor (α)**
- **Covariance of temperature gradient was obtained for ^{238}U neutron capture in the JFS-60 group structure.**
- **Contribution of uncertainty of temperature gradient of self-shielding factor to a 600 MWe FBR is about 0.23% (total:3.5%)**